

FEDERAL TECHNOLOGY ALERTS

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Non-Chemical Technologies for Scale and Hardness Control

Technology for improving energy efficiency through the removal or prevention of scale.

Abstract

The magnetic technology has been cited in the literature and investigated since the turn of the 19th century, when lodestones and naturally occurring magnetic mineral formations were used to decrease the formation of scale in cooking and laundry applications. Today, advances in magnetic and electrostatic scale control technologies have led to their becoming reliable energy savers in certain applications.

For example, magnetic or electrostatic scale control technologies can be used as a replacement for most water-softening equipment. Specifically, chemical softening (lime or lime-soda softening), ion exchange, and reverse osmosis, when used for the control of hardness, could potentially be replaced by non-chemical water conditioning technology. This would include applications both to cooling water treatment and boiler water treatment in once-through and recirculating systems.

The primary energy savings from this technology result from decrease in energy consumption in heating or cooling applications. This savings is associated with the prevention or removal of scale build-up on a heat exchange surface, where even a thin film can increase energy consumption by nearly 10%. Secondary energy savings can be attributed to reducing the pump load, or system pressure, required to move the water through a scale-free, unrestricted piping system.

This *Federal Technology Alert* provides information and procedures that a Federal energy manager needs to evaluate the cost-effectiveness of this technology. The process of magnetic or eletrostatic scale control and its energy savings and other benefits are

explained. Guidelines are provided for appropriate application and installation. In addition, a hypothetical case study is presented to give the reader a sense of the actual costs and energy savings. A listing of current manufacturers and technology users is provided along with references for further reading.

About the Technology

The technology addressed in this FTA uses a magnetic or electrostatic field to alter the reaction between scale-forming ions in hard water. Hard water contains high levels of calcium, magnesium, and other divalent cations. When subjected to heating, the divalent ions form insoluble compounds with anions such as carbonate. These insoluble compounds have a much lower heat transfer capability than heat transfer surfaces such as metal. They are insulators. Thus additional fuel consumption would be required to transfer an equivalent amount of energy.

The magnetic technology has been cited in the literature and investigated since the turn of the 19th century, when lodestones or naturally occurring magnetic mineral formations were used to decrease the formation of scale in cooking and laundry applications.

However, the availability of high-power, rare-earth element magnets has advanced the magnetic technology to the point where it is more reliable. Similar advances in materials science, such as the availability of ceramic electrodes and other durable dielectric materials, have allowed the electrostatic technology to also become more reliable.

The general operating principle for the magnetic technology is a result of the physics of interaction between a magnetic field and a moving electric charge, in this case in the form of an ion. When ions pass through the magnetic field, a force is exerted on each ion. The forces on ions of opposite charges are in opposite directions. The redirection of the particles tends to increase the frequency with which ions of opposite charge collide and combine to form a mineral precipitate, or insoluble compound. Since this reaction takes place in a low-temperature region of a heat exchange system, the scale formed is non-adherent. At the prevailing temperature conditions, this form is preferred over the adherent form, which attaches to heat exchange surfaces.

The operating principles for the electrostatic units are much different. Instead of causing the dissolved ions to come together and form non-adherent scale, a surface charge is imposed on the ions so that they repel instead of attract each other. Thus the two ions (positive and negative, or cations and anions, respectively) of a kind needed to form scale are never able to come close enough together to initiate the scale-forming reaction. The end result for a user is the same with either technology; scale formation on heat exchange surfaces is greatly reduced or eliminated.

Application Domain

These technologies can be used as a replacement for most water-softening equipment. Specifically, chemical softening (lime or lime-soda softening), ion exchange, and reverse osmosis (RO), when used for the control of hardness, can be replaced by the non-chemical water conditioning technology. This would include applications both to cooling water treatment and boiler water treatment, in once-through and recirculating systems. Other applications mentioned by the manufacturers include use on petroleum pipelines as a means of decreasing fouling caused by wax build-up, and the ability to inhibit biofouling and corrosion.

The magnetic technology is generally not applicable in situations where the hard water contains "appreciable" concentrations of iron. In this FTA, appreciable means a concentration requiring iron treatment or removal prior to use, on the order of parts per million or mg/L. The reason for this precaution is that the action of the magnetic field on the hardness-causing ions is very weak. Conversely, the action of the magnetic field on the iron ions is very strong, which interferes with the water conditioning action.

A search of the Thomas Register™ in conjunction with manufacturer contact yielded eleven manufacturers of magnetic, electromagnetic or electrostatic water conditioning equipment that fell within the scope of this investigation. The defined scope includes commercial or industrial-type magnetic, electromagnetic or electrostatic devices marketed for scale control. Devices intended for home use, as well as other non-chemical means for scale control, such as reverse osmosis, are not within the extended scope of this FTA.

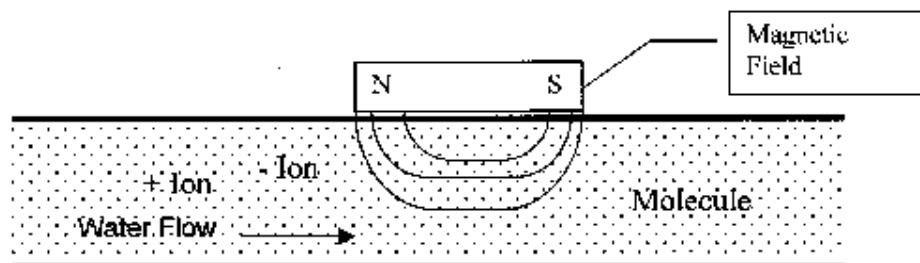


Figure 1. Diagram of General Magnetic Device Construction

Exact numbers of units deployed by these manufacturers are virtually impossible to compile, as some of the manufacturers had been selling the technology for up to 40 years. One manufacturer claims as many as 1,000,000 units (estimated total of all manufacturers represented here) are installed in the field. Where not withheld by the manufacturer because of business sensitivity reasons, customer lists included both Federal and non-Federal installations. Those manufacturers who did withhold the customer list indicated a willingness to disclose customer contacts to legitimate prospective customers.

Literature provided by and discussions with manufacturers described a typical installation for a boiler water treatment scheme as including the device installed upstream of the boiler. Manufacturers vary in their preference of whether the device should be installed close to the water inlet or close to the boiler. Both locations have been documented as

providing adequate performance. Generally, the preferred installation location for use with cooling towers or heat exchangers is upstream of the heat exchange location and upstream of the cooling tower. Downstream of the cooling tower but upstream of the heat source was also mentioned as a possible installation location, primarily for the use with chillers or other cooling equipment.

The primary *caveat* on installation of the magnetic technology is that high voltage (230V, 3-phase or above) power lines interfere with operation by imposing a second magnetic field on the water. (This is most noticeable when these electric power sources are installed within three feet of a magnetic device.) This second magnetic field most likely will not be aligned with the magnetic field of the device, thus introducing interference and reducing the effectiveness of the treatment. Installations near high voltage power lines are to be avoided if possible. Where avoidance is not possible, the installation of shielded equipment is recommended to achieve optimum operation. Some manufacturers also have limitations on direction of installation--vertical or horizontal--because of internal mechanical construction.

Energy-Savings Mechanism

The primary energy savings result from a decrease in energy consumption in heating or cooling applications. This savings is associated with the prevention or removal of scale build-up on a heat exchange surface where even a thin film (1/32" or 0.8 mm) can increase energy consumption by nearly 10%. Example savings resulting from the removal of calcium-magnesium scales are shown in Table 1. A secondary energy savings can be attributed to reducing the pump load, or system pressure, required to move the water through a scale-free, unrestricted piping system.

**Table 1. Example Increases in Energy Consumption
as a Function of Scale Thickness**

Scale Thickness (inches)	Increased Energy Consumption (%)
1/32	8.5
1/16	12.4
1/8	25.0
1/4	40.0

As was discussed above, magnetic and electric fields interact with a resultant force generated in a direction perpendicular to the plane formed by the magnetic and electric field vectors. (See Figure 2 for an illustration.) This force acts on the current carrying entity, the ion. Positively charged particles will move in a direction in accord with the Right-hand Rule, where the electric and magnetic fields are represented by the fingers and the force by the thumb. Negatively charged particles will move in the opposite direction. This force is in addition to any mixing in the fluid due to turbulence.

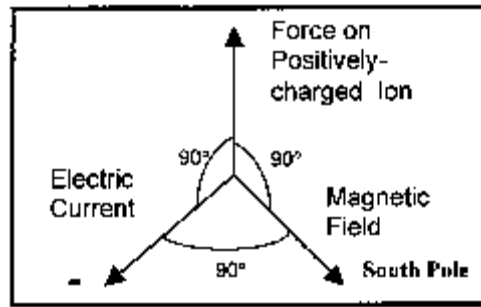


Figure 2. Diagram Showing Positioning of Fields and Force

The result of these forces on the ions is that, in general, positive charged ions (calcium and magnesium, primarily) and negative charged ions (carbonate and sulfate, primarily) are directed toward each other with increased velocity. The increased velocity should result in an increase in the number of collisions between the particles, with the result being formation of insoluble particulate matter. Once a precipitate is formed, it serves as a foundation for further growth of the scale crystal. The treatment efficiency increases with increasing hardness since more ions are present in solution; thus each ion will need to travel a shorter distance before encountering an ion of opposite charge.

A similar reaction occurs at a heat exchange surface but the force on the ions results from the heat input to the water. Heat increases the motion of the water molecules, which in turn increases the motion of the ions, which then collide. In addition, scale exhibits an inverse solubility relationship with temperature, meaning that the solubility of the material decreases as temperature increases. Therefore, at the hottest point in a heat exchanger, the heat exchange surface, the scale is least soluble, and, furthermore due to thermally induced currents, the ions are most likely to collide nearest the surface. As above, the precipitate formed acts as a foundation for further crystal growth.

When the scale-forming reaction takes place within a heat exchanger, the mineral form of the most common scale is called calcite. Calcite is an adherent mineral that causes the build-up of scale on the heat exchange surface. When the reaction between positively charged and negatively charged ions occurs at low temperature, relative to a heat exchange surface, the mineral form is usually aragonite. Aragonite is much less adherent to heat exchange surfaces, and tends to form smaller-grained or softer-scale deposits, as opposed to the monolithic sheets of scale common on heat exchange surfaces.

These smaller-grained or softer-scale deposits are stable upon heating and can be carried throughout a heating or cooling system while causing little or no apparent damage. This transport property allows the mineral to be moved through a system to a place where it is convenient to collect and remove the solid precipitate. This may include removal with the wastewater in a once-through system, with the blowdown in a recirculating system, or from a device such as a filter, water/solids separator, sump or other device specifically introduced into the system to capture the precipitate.

Water savings are also possible in recirculating systems through the reduction in blowdown necessary. Blowdown is used to reduce or balance out the minerals and chemical concentrations within the system. If the chemical consumption for scale control is reduced, it may be possible to reduce blowdown also. However, the management of corrosion inhibitor and/or biocide build-up, and/or residual products or degradation by-products, may become the controlling factor in determining blowdown frequency and volume.

Other Benefits

Aside from the energy savings, other potential areas for savings exist. The first is elimination or significant reduction in the need for scale and hardness control chemicals. In a typical plant, this savings could be on the order of thousands of dollars each year when the cost of chemicals, labor and equipment is factored in. Second, periodic descaling of the heat exchange equipment is virtually eliminated. Thus process downtime, chemical usage, and labor requirements are eliminated. A third potential savings is from reductions in heat exchanger tube replacement due to failure. Failure of tubes due to scale build-up, and the resultant temperature rise across the heat exchange surface, will be eliminated or greatly reduced in proportion to the reduction in scale formation.

Variations

Devices are available in two installation variations and three operational variations. First to be discussed are the two installation variations: invasive and non-invasive. Invasive devices are those which have part or all of the operating equipment within the flow field. Therefore, these devices require the removal of a section of the pipe for insertion of the device. This, of course, necessitates an amount of time for the pipe to be out of service. Non-invasive devices are completely external to the pipe, and thus can be installed while the pipe is in operation. Figure 3 illustrates the two installation variations.

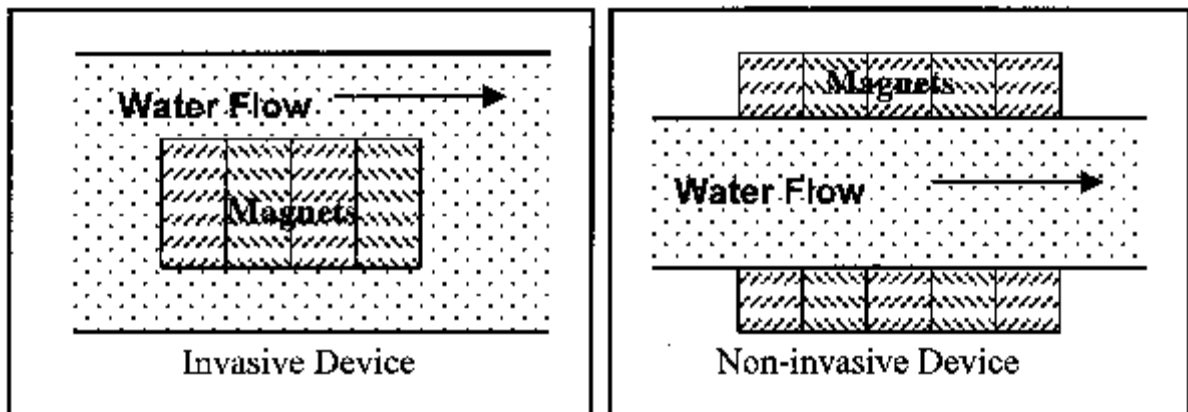


Figure 3. Illustration of Classes of Magnetic Devices by Installation Location

The operational variations have been mentioned above; illustrations of the latter two types are shown Figure 4:

Magnetic, more correctly a permanent magnet

Electromagnetic, where the magnetic field is generated via electromagnets

Electrostatic, where an electric field is imposed on the water flow, which serves to attract or repel the ions and, in addition, generates a magnetic field.

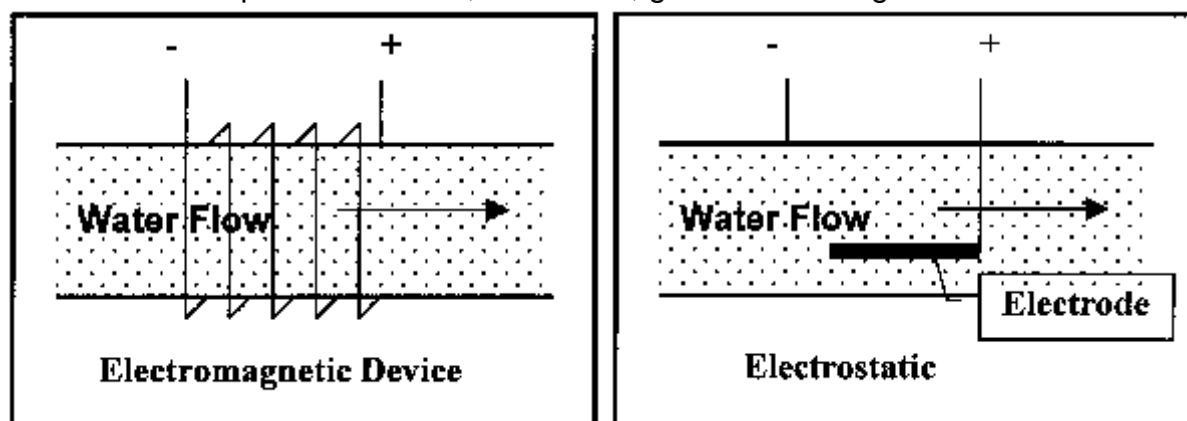


Figure 4. Illustration of Classes of Non-Permanent Magnet Devices

Electrostatic units are always invasive. The other two types can be either invasive or non-invasive. The devices illustrated in Figure 3 are examples of permanent magnet devices.

Installation

Most of the devices are in-line--some invasive, some non-invasive--as opposed to side-stream. The invasive devices require a section of pipe to be removed and replaced with the device. Most of the invasive devices are larger in diameter than the section of pipe they replace. The increased diameter is partially a function of the magnetic or electromagnetic elements, and also a function of the cross sectional flow area. The flow area through the devices is generally equivalent to the flow area of the section of pipe removed.

The non-invasive in-line devices are designed to be wrapped around the pipe. Thus downtime, or line out-of-service time, is minimized or eliminated.

Federal Sector Potential

The potential cost-effective savings achievable by this technology were estimated as part of the technology assessment process of the New Technology Demonstration Program (NTDP).

Technology Screening Process

New technologies were solicited for NTDP participation through advertisements in the

Commerce Business Daily and trade journals, and, primarily, through direct correspondence. Responses were obtained from manufacturers, utilities, trade associations, research institutes, Federal sites and other interested parties. Based on these responses, the technologies were evaluated in terms of potential Federal-sector energy savings and procurement, installation, and maintenance costs. They were also categorized as either just coming to market ("unproven" technologies) or as technologies for which field data already exist ("proven" technologies). The energy savings and market potentials of each candidate technology were evaluated using a modified version of the Facility Energy Decisions Screening (FEDS) software too (Dirks and Wrench, 1993).

Non-chemical water treatment technologies were judged life-cycle cost-effective (at one or more Federal sites) in terms of installation cost, net present value, and energy savings. In addition, significant environmental savings from the use of many of these technologies are likely through reductions in CO₂, NO_x, and SO_x emissions.

Estimated Savings and Market Potential

As part of the NTDP selection process, an initial technology screening activity was performed to estimate the potential market impact in the Federal sector. Two technologies were run through the assessment methodology. The first technology was assessed assuming the technology was applied to the treatment of boiler make-up water. The second technology was assessed assuming the technology was applied to both the treatment of boiler make-up water and cooling tower water treatment. The technology screenings used the economic basis required by 10 CFR 436. The costs of the two technologies were different based on information provided by the manufacturers, thus leading to different results.

The technologies were ranked on a total of ten criteria. Three of these were financial, including net present value (NPV), installed cost, and present value of savings. One criterion was energy-related, annual site energy savings. The remaining criteria were environmental and dealt with reductions in air emissions due to fuel or energy savings and included SO₂, NO_x, CO, CO₂, particulate matter and hydrocarbon emissions. The ranking results from the screening process for this technology are shown in Table 2. These values represent the maximum benefit achieved by implementation of the technology in every Federal application where it is considered life-cycle cost-effective. The actual benefit will be lower because full market penetration is unlikely to ever be achieved.

Table 2. Screening Criteria Results

Screen Criteria	Results	
	First Screen	Second Screen
Net Present Value (\$)	147,518,000.	158,228,000.

Installed Cost (\$)	52,819,000.	35,299,000.
Present Value of Savings (\$)	200,336,000.	193,527,000.
Annual Site Energy Savings (Mbtu)	4,166,000.	3,761,000.
SO ₂ Emissions Reduction (lb/yr)	3,292,000.	427,000.
NO _x Emissions Reduction (lb/yr)	1,028,000.	550,000.
CO Emissions Reduction (lb/yr)	304,000.	128,000.
CO ₂ Emissions Reduction (lb/yr)	303,000.	234,000.
Particulate Emissions Reduction (lb/yr)	60,000.	29,000.
Hydrocarbon Emissions Reduction (lb/yr)	7,000.	3,000.
Note: First Screen: Boiler make-up water treatment. Second Screen: Cooling tower water treatment and boiler make-up water treatment.		

Laboratory Perspective

The primary question to be answered is "Does the technology work as advertised?" The history of the technologies, as illustrated through primarily qualitative--but some quantitative--assessment in many case studies, has shown that when properly installed, a decrease in or elimination of scale formation will be found. While the evidence supporting the technologies may be thought of as mainly anecdotal, the fact remains that upon visual inspection after installation of these devices the formation of new scale deposits has been inhibited. In addition, in most cases, scale deposits present within the system at the time of installation have been removed.

The key here is *properly installed*. By this it is meant that a manufacturer or their qualified representative is responsible for equipment integration. Unlike many other technologies where much of the knowledge has been reduced to a quantitative model, the non-chemical water treatment industry still relies largely on experience as the means of providing quality installation, service and, consequently, customer satisfaction. Of particular interest to the manufacturer would be physical parameters such as water flow rate, and water quality parameters such as hardness, alkalinity, and iron concentration. These parameters will help determine the optimum size and the extent of treatment.

The manufacturer may also want to know whether the installation is for use in conjunction with a boiler or a cooling tower, and for once-through or recirculating water systems. These parameters will help determine the optimum location within the system. Other factors of interest may include whether the cooling or heating system is sensitive to particulate matter, and if so what particle sizes. The device works by initiating the precipitation of scale, thus particulate matter will be present in the treated water. If the system is sensitive to particulate matter there may be a need for a solid separation device

such as a filter, a settling basin, a cyclone, or a sump to collect solids and to allow for their easy removal from the system.

Application

This section addresses the technical aspects of applying the technology. The range of applications and climates in which the technology can be applied are addressed. The advantages, limitations, and benefits in each application are enumerated. Design and integration considerations for the technology are discussed, including equipment and installation costs, installation details, maintenance impacts, and relevant codes and standards. Utility incentives and support are also discussed.

Application Screening

As mentioned previously, the technology can be applied wherever hard water is found to cause scale. Since the technology is a physical process, as opposed to chemical water softening, it is expected to perform best in locations with harder water. In general, only a few locations do not require or would not benefit from some type of hardness control. Hard water is one in which the hardness is greater than 60 mg/L (or ppm) as calcium carbonate. This corresponds to approximately 3.5 grains of hardness per U.S. gallon. The Pacific Northwest states, the North Atlantic coastal states, and the Southeast states, excluding Florida, are locations where naturally occurring soft water is most likely to be found. The balance of the United States could benefit from some type of water treatment to control scale formation, using either one of the traditional technologies such as lime softening or ion exchange, or the non-chemical technology discussed in this FTA.

Where to Apply

Non-chemical scale control technologies can be used for either boiler scale control or cooling tower scale control. Boiler scale control applications are the majority of the installations, but the control of silica scale in cooling water applications is also possible. Experience has been cited with both retrofit installations and in new installations (see References for a brief listing of applicable reports and publications).

Non-chemical scale control technologies are best applied:

- When the use of chemicals for water treatment is to be minimized or eliminated. Lime, salt and acid for cleaning can be reduced or eliminated.

- When space requirements do not allow installation of lime softening equipment or ion exchange equipment. The non-chemical technologies are generally very space efficient.

When particulate matter in the water can be tolerated by the process; otherwise solids separation is required.

When frequent system shutdowns are required for descaling even with a diligent chemical scale control program.

In remote locations where delivery of chemicals and labor cost makes conventional water softening or scale control methods cost prohibitive.

What to Avoid

There are a few precautions to be noted before selecting the technology:

This technology is littered with disreputable manufacturers or vendors, the actions of whom have given the technology an undesirable history in the eyes of many. Work with a reputable manufacturer (such as those included herein) through their engineering department or their designated installer. These people have much more experience with the technology than the typical water treatment engineering firm.

Be aware of process water requirements since these requirements may dictate the need to install solids separation equipment or iron removal equipment in order to maximize the performance of the technology.

Installation near high voltage electrical equipment or strong magnetic fields is to be avoided since these fields will interfere with the performance of the technology. (Near is relative to the voltage; for 208/220/240V it means within 36 inches; for higher voltages it is proportionally more distant.) Also, check the pipeline for its use as an electrical ground. Stray electrical current in the pipe will have the same effect as installation near a strong electrical or magnetic field.

Installation

Installation issues with these devices are few. The first issue is whether a permanent magnet or one of the electronic devices is chosen. The latter needs a suitable supply of electricity.

The second issue is device capacity, which will dictate space requirements and pipe size. The pipe size generally determines the fittings. Smaller devices, up to approximately 2" pipe size, are available with solder or pipe thread fittings. Larger devices may have flange fittings that would necessitate the installation of matching flanges in the current pipe arrangement.

The third issue is the potential for downtime, which needs to be coordinated with other facility activities. However, this should not be a major impediment since downtime for cleaning and maintenance of cooling towers, or boiler inspection is part of the regularly scheduled activities for most installations.

A fourth issue would arise with the corrosion control chemistry, which will likely need some adjustment under a non-chemical scale control technology. In many cases the layer

of scale on heat transfer surfaces is beneficial from a corrosion control standpoint. With this layer not present when using a non-chemical technology, the concentration of corrosion control chemicals may need adjustment in order to provide the proper protection. On the reverse side, many users are claiming the presence of a fine powdery film on the surfaces the treated water contacts. This powder has been attributed to serve as a corrosion inhibitor.

The most significant issue may be whether a solids separation device is needed to remove the particulates formed. Filters, hydrocyclones, and settling basins are all compatible with the technology. The choice among these or other solids separation technologies should be made in conjunction with the manufacturer who will have the best idea of particle size distribution, and thus the relative efficiencies of the separation technologies.

Maintenance Impact

There is a significant, positive impact on maintenance. Field applications have shown the technology to be capable of controlling scale for extended periods of time, months or years, eliminating the periodic cleaning or descaling of process equipment that is typical of conventional, chemical-based scale control technologies. The resources--time, chemicals, and equipment--previously devoted to periodic scale removal from heat exchange surfaces will be made available for other tasks. Note, however, the need for periodic inspection of the heat exchange surfaces is not reduced or eliminated.

The electrostatic devices also require periodic inspection of the electrodes. This scheduled maintenance activity can be performed in conjunction with the heat exchange surface inspection and requires less than a person-day to disassemble and inspect the system.

Equipment Warranties

All of the manufacturers offer some type of warranty on their respective device. The range is from 90 days to as much as 10 years. Another perspective is the potential impact upon warranties for installed equipment. No information was uncovered as part of this effort to indicate any instance where a boiler or cooling tower equipment manufacturer voided a warranty for equipment. However, no specific effort was made to contact manufacturers of boilers and cooling tower equipment to assess specific warranty conditions or policies.

Codes and Standards

Only one code or standard specific to the non-chemical technologies was identified in the course of preparing this FTA: API 960, Evaluation of the Principles of Magnetic Water Treatment, 09/1985, 89 pages. Of course, all applicable plumbing, piping, mechanical, and/or electrical

codes and standards would still apply.

Costs

Cost information was requested from each manufacturer for three different-size units, based on flow rate: 1 gpm (gallons per minute), 100 gpm and 1,000 gpm. As is typical of process equipment, cost per unit of treatment decreases with increasing capacity. To treat 1 gpm, a typical cost was on the order of \$100, or about \$100 per gpm. To treat 1,000 gpm a typical cost was on the order of \$10,000, or about \$10 per gpm.

In general, the electronic units were more costly than the magnetic units for an equivalent flow rate. Costs also ranged considerably with unit size, with the 1-gpm units ranging in cost up to \$500. For the 1,000-gpm units the range of costs was considerably greater, from \$900 to over \$1,000,000.

Installation costs also varied widely, in conjunction with equipment size. The lower flow rate units will mate with 3/4" to 1" pipe sizes with soldered, flanged or threaded (NPT) fittings. Installation time estimates were on the order of one hour, with additional parts costing less than \$10. The larger-size units (1,000 gpm) were typically designed to mate with a 12" to 18" pipe using a flange fitting. Estimated installation time ranged from one to four person-days, requiring less than \$1,000 in additional materials.

Weight was an important characteristic in the installation estimate because the permanent magnet units may exceed 1,000 pounds. There is a trade-off between installing a heavier permanent magnet unit requiring no outside power versus a lighter electronic unit for which an electrical connection needs to be made, and possibly electrical lines run to the point of installation. The net effect is expected to be neutral with regard to installation time estimates.

Since these units are typically delivered in the sizes quoted off-the-shelf, there is no design cost by the manufacturer. Facilities engineering and design for calculations and updating plant drawings should amount to less than two person-days for the large units, and less than an hour for the small units.

Utility Incentives and Support

Although no specific incentive programs were identified, the Department of Energy and the Advanced Research Projects Agency have funded research in this area. Some utility or trade associations have supported the electronic technologies with funds and exposure. For example, the American Water Works Association sponsored a conference to discuss the non-traditional treatment technologies. In addition, as California municipalities face water shortages, they have turned to a number of measures to lower water consumption and increase water quality. Many have prohibited the use of water softeners and may offer assistance infunding conversion to low/no salt water conditioning technologies.

Additional Considerations

There are additional considerations to be taken into account. Primary among these is the reduction in chemical use at the facility for water softening. The chemical use reduction may lead to reduced safety, training and reporting requirements.

Electricity consumption will also be reduced. The actual reduction is highly dependent upon the technology employed. Permanent magnets use no electricity, so both the on-site electricity used for chemical treatment as well as the off-site energy required to produce and transport the chemicals will be eliminated. For the electronic units, on-site energy requirements may vary from as little as 10% of the chemical-based treatment system energy consumption--typical, to 10 times the energy consumed by the chemical-based treatment system.

Energy consumption reductions will lead directly to reductions in air combustion emissions. There will also be additional indirect reductions due to decreased transportation of fuels and decreased fuel processing. The latter will also lead to reductions in water use, water pollution, and solid wastes from mining and processing operations.

Technology Performance

The information in this section was compiled primarily from case studies, along with selected contact with users and third party researchers. As mentioned previously, the use of magnetic or electric fields to treat water had its origins near the turn of the 19th century. Commercialization of the technology began after World War II, with the largest advances coming in the last 20 years with the development of rare earth magnets and inexpensive electronic controls.

There are records of installation of the technology in the United States from about 1950. Manufacturers claim to have installations operating satisfactorily for as long as 30 years. No good statistics were available on the total number of installations over this period. However, using the estimates of one manufacturer as a basis, there could be upwards of 1,000,000 units installed in the United States in commercial or industrial facilities, inclusive of all units installed by all manufacturers.

Field Experience

As has been alluded to above, user experience has been positive. Two experiences have been common. First, users have noted a dramatic reduction in scale formation to the point where the need for chemical scale control is eliminated. Second, the prior build-up of scale on heat exchange surfaces has been removed over time. This last process has been noted as taking from

30 days to over a year, depending upon the thickness and composition of the scale.

This is not to say there have not been less than successful installations or applications. The non-chemical technologies may not be universally applicable for scale control, just as any technology may not be a universally applicable solution to the problem it was designed to solve.

The magnetic technologies are not as effective when silica is present in the system. Nor do they work as efficiently when iron is present, as was mentioned above, or when other magnetic minerals are present. The history of the technology is also littered with cases where the magnet field was applied incorrectly or did not have sufficient strength to affect the reaction. This latter was especially true early in the life cycle of the technology when ferrous-based magnets were the norm. High levels of particulate matter will also negatively influence the efficiency of the technology by reducing the collision frequency of the desirable reactions.

Energy Savings

Energy savings result from both reductions in pumping energy input to the system and reduction in fuel consumption. The first aspect has not been well quantified by the users or in any of the case studies. It is thought of as a secondary benefit.

Fuel consumption has been lowered in every situation. The exact savings are a result of a number of factors:

- How effective the chemical scale control program may have been relative to the input water hardness

- How often the heat exchange system was taken down for maintenance and cleaning.

On systems that were descaled frequently or had low scale formation, due to low hardness and/or an effective chemical scale control program, the savings in fuel consumption was lower, often from a few percent to as much as 15%. The lower savings were at an installation using ion exchange softening of moderately hard water (less than 150 mg/L as calcium carbonate hardness). On systems where descaling was infrequent or absent altogether, or where the chemical scale control program was not as effective in controlling scale formation, fuel consumption savings ranged up to 30%. This was found to be the case in an installation using very hard water (hardness in excess of 300 mg/L as calcium carbonate), and a chemical scale control program, with heat exchanger tubes closing due to scale formation after less than one year. In each case the fuel consumption savings was proportional to the thickness of the scale layer removed.

One important note was that fuel consumption savings often trailed installation of the technology by a significant period due to the fact that the savings is driven by the amount of scale on the heat exchange surface. The accumulated scale will erode over time, resulting in fuel consumption reductions. For this reason, many of the manufacturers

recommend installing the technology only after the system has been descaled, thus savings in fuel consumption would be immediate.

Maintenance

As mentioned above, maintenance requirements typically are reduced upon implementation of the non-chemical technology. First, periodic maintenance of the water-softening equipment and chemicals is eliminated. Second, the periodic heat exchanger inspection and cleaning cycle is reduced to an inspection cycle. The handling and storage requirements for the chemicals--lime, soda ash, salt and acid--have been eliminated, as has training for their use, storage and handling. The reduction in these periodic activities frees up the previously time allocated for application to other activities.

There are maintenance activities associated with this technology. For the electromagnetic and electrostatic units, a daily check that the power is on is necessary (a "power on" indicator light is included with most, if not all, units). The electrostatic units need to have the electrodes checked periodically, semi-annually, and the electrodes replaced when noticeably worn or damaged, perhaps every five years. The reader should speak to the manufacturer for details which may vary.

When solids or particulates accumulate in the system, they will need to be removed. Automatic blowdown of the system should control the daily accumulation. If the system is not cleaned prior to installation of the non-chemical technology, the scale in the system will detach and its removal will be necessary. Filters, sumps and hydrocyclones are all effective means of capturing the solids, but each will require periodic cleaning.

Environmental Impacts

There are areas where the technology mitigates environmental impacts. The first is air quality due to emissions reduction associated with decreases in fuel consumption. The second is a corresponding decrease in solid wastes, ash and other fuel combustion residues to be disposed. Of course, this will only be applicable in the situation in which an end user combusts fuels on-site for the production of power. A third area is the reduction in release, or potential for release, of water treatment chemicals stored at a facility. Since chemical consumption will decrease, emissions from storage will also decrease. The wastes associated with disposal and management of used chemical containers will also be reduced.

Case Study

For the case study, a hypothetical facility is used and the application of a permanent magnet device is described. The conditions are based on information gathered during the user interviews

and reading of published and unpublished case studies. The purpose is to illustrate the types of data required to prepare a site-specific cost analysis, not to illustrate what any particular user might experience in the way of cost savings.

Facility Description

The facility currently uses extremely hard water (hardness of 350 mg/L as calcium carbonate) and employs lime softening. The process water is used in a recirculating boiler water system with flow of 1,000 gpm or 1.4 MGD (million gallons per day). Makeup and blowdown were estimated at 10% of the flow, or 140,000 gallons per day. The water-softening process removes a significant fraction of the hardness, but not all, leading to semiannual inspections and annual cleaning of the heat exchanger. This frequency is thought to be fairly typical.

Cost for the lime used in the process is estimated at \$10/ton delivered. Cost for natural gas is \$5.80/1000 ft³. Acetic acid, used for cleaning, costs \$2 per gallon.

Existing Technology Description

The current system is a conventional lime softening plant consisting of lime storage facilities, a slaker where the powered lime is mixed with water, a mixing basin for adding controlled amounts of the lime solution to the water, and a settling basin where the precipitated solids are removed. Downstream of the water treatment facilities is a conventional shell-and-tube heat exchanger used to heat the water for both building heat and process water.

Lime consumption for softening is 48 tons/year. In this case, alkalinity is sufficient so as to not require the addition of soda ash during the softening process. Natural gas consumption for process water heating is 400,000 MBtu/year. Electricity consumption for the softening process was estimated at 3,100 kWh per year. Acetic acid is used during cleaning, approximately 100 gallons per cleaning. Production losses due to system downtime are not being included in this analysis.

(If the system had instead used ion exchange softening, the applicable chemical use information would have been the regenerant, typically salt but possibly acid, and the consumption of ion exchange resin. This last item is calculated as the mass replaced divided by the total volume of water treated.)

Data on lime consumption can typically be found in purchasing records, or also in a water treatment system operator's log. The latter would be more accurate since it would more closely reflect lime used for water softening, whereas the former would list only lime purchases including those for water softening, pH adjustment and other uses.

Natural gas consumption, or other fuel consumption data, can be taken from accounting records, if the only use of natural gas is for process water, or from operation data, (e.g., firing rate data), or calculated from an energy balance for a portion of the production

system. The firing rate data or other operation data would be the most accurate but might not always be available.

Electricity consumption information can be calculated from nameplate capacity of the mixing and pumping equipment involved. For this report, it was derived from information compiled by the Electric Power Research Institute. In some cases there may be energy or monitoring data available for the process that would be available as part of the water treatment system operator's records.

New Technology Equipment Selection

A magnetic scale control device will be investigated as an alternative to chemical scale control. The first step was consultation with the manufacturer, including submitting water analysis data and a schematic of the current system showing the proposed location of the equipment to facilitate manufacturer selection and equipment sizing. (A magnetic device was chosen because the preferred installation location was remote, with electrical power not readily available.)

For the proposed location and required flow rate, a unit was identified that would fit the current piping configuration without a need for adapters. The unit cost is \$10,000 including shipping. The estimate by the in-house facilities engineering staff calls for three days to install the system, one-half day each for set-up and clean-up, one day to remove a section of pipe to make space for the device (including installing flanges), and one day for installation and leak testing. Three people are required, as well as a device capable of lifting 1,000 pounds in order to position the device and facilitate removal of the old section of pipe.

One of the key elements to sizing these devices is the water velocity through the device. Manufacturers recommend, typically, at least a 7 feet per second water velocity. If the water velocity through a section of pipe is too low, it will be necessary to use adapters to decrease the size of the pipe through the device, thus increasing the velocity. Water velocity in feet per second can be calculated as follows, where *Diameter* is in feet:

$$U = \frac{0.535 * \text{GPM}}{\pi * \text{Diameter}^2}$$

Savings are expected to result from discontinuance of chemical consumption and decreased energy consumption (10% of process energy and all of the water treatment energy). Inspection will still occur.

Savings Potential

Energy savings can result from two areas. First is the reduction in fuel used in generating heat. Methods for calculating the fuel consumption were discussed above in the technology descriptions. The fuel consumption savings is simply the net difference, in this case estimated equal to 10% of the baseline fuel consumption. (This estimated savings was used to illustrate a

case where there was a fairly uniform 1/16" thick layer of scale across a heat exchanger surface. Of course, it is realized that the scale layer, and therefore energy consumption, builds over time and is not an instantaneous effect.) This savings is also equal to the loss in heat transfer efficiency due to scale formation on the heat exchange surface.

Second is the energy savings resulting from decreased pressure drop within the heat exchanger. This is not quantified here, but could be quantified if the pressure drop through the current system was known, along with the energy characteristics of the pump so that reductions in pressure could be related to energy consumption.

Cost savings also result from reductions in chemical use. Chemical softening will be reduced, and likely eliminated, by the use of non-chemical treatment technologies. There will also be a corresponding energy decrease from the shutdown of chemical mixing equipment and water treatment equipment used in the softening process. The estimated chemical savings here was 480 tons per year and the corresponding electricity savings was 31,000 kWh per year.

Table 3 illustrates typical consumption data for the baseline and alternative and the potential annual costs savings. Not shown are water consumption and water discharge, which do not change between the alternatives. Capital cost for the alternative treatment system, estimated at \$10,000 at the beginning of the 15-year analysis period, is not shown either. Fifteen years was chosen because it was typical of the life of field units.

Table 3. Annual Costs and Savings

Item	Cost \$/unit	Baseline Lime Softening		Alternative Magnetic Treatment		Annual Costs Savings
		Annual Consumption	Annual Cost \$/year	Annual Consumption	Annual Cost \$/year	
Electricity						
Natural	0.05/kWh	3,100	155	0	0	155
Gas	5.80/MBtu	400,000	2,320,000	360,000	2,088,000	232,000
Chemicals	10/ton	48	480	0	0	480
Total			2,320,635		2,088,000	232,635

Life-Cycle Cost

The full results of the BLCC computations are shown in Appendix B. A discussion of the BLCC software is given in Appendix A. The BLCC Comparative Economic Analysis is shown in Figure 5. Installation cost for the magnetic treatment device is estimated at \$10,360, calculated as \$10,000 for the device and \$360 for design and installation labor. Operating costs for the

technology are estimated at \$2,088,000 per year versus costs of \$2,320,635 per year for the conventional lime-softening technology, both exclusive of water consumption and discharge. Life-cycle costs for each of the technologies as calculated by the BLCC software are \$27,524,500 for the magnetic technology versus \$30,283,500 for the conventional technology. (This includes the cost of water and wastewater disposal of \$2,605,292.) This represents a life-cycle cost savings of \$2,759,000. The Simple Payback from BLCC is less than one year, and the Adjusted Internal Rate of Return is 50.66%.

N I S T B L C C: COMPARATIVE ECONOMIC ANALYSIS (ver. 4.4-97)

Project: Non-Chemical Scale Control FTA

Base Case: Lime Soft.

Alternative: Magnetic

Principal Study Parameters:

Analysis Type: Federal Analysis-Energy Conservation Projects

Study Period: 15.00 Years (NOV 1997 through OCT 2012)

Discount Rate: 3.8% Real (exclusive of general inflation)

Base Case LCC File: SOFTEN.LCC

Alternative LCC File: MAGNETIC.LCC

Comparison of Present-Value Costs

	Base Case: Lime Soft.	Alternative: Magnetic	Savings from Alt.
Initial Investment item(s):			
Capital Requirements as of Serv. Date	\$0	\$10,360	-\$10,360
Subtotal	\$0	\$10,360	-\$10,360
Future Cost Items:			
Energy-related Costs	\$27,678,200	\$24,908,850	\$2,769,350
Water Costs	\$2,605,292	\$2,605,292	\$0
Subtotal	\$30,283,500	\$27,514,140	\$2,769,360
Total P.V. Life-Cycle Cost	\$30,283,500	\$27,524,500	\$2,759,000

Net Savings from Alternative 'Magnetic' compared to Base Case 'Lime Soft.'

Net Savings = P.V. of Non-Investment Savings \$2,769,360

- Increased Total Investment \$10,360

Net savings: \$2,759,000

Note: the SIR and AIRR computations include differential initial costs, capital replacement costs, and residual value (if any) as investment costs, per NIST Handbook 135 (Federal and MILCON analyses only).

Savings-to-Investment Ratio (SIR)

For Alternative 'Magnetic' compared to Base Case 'Lime Soft.'

$$SIR = \frac{\text{P.V. of non-investment savings}}{\text{Increased total investment}} = 267.31$$

Adjusted Internal Rate of Return (AIRR)

For Alternative 'Magnetic' compared to Base Case 'Lime Soft.'

(Reinvestment Rate = 3.80%; Study Period = 15 years)

AIRR = 50.66%

Estimated Years to Payback

Simple Payback occurs in year 1

Discounted Payback occurs in year 1

ENERGY SAVINGS SUMMARY

Energy type	Units	Average Annual Consumption			Life-Cycle Savings
		Base Case	Alternative	Savings	
Electricity	kWh	3,100.0	0.0	3,100.0	46,500.0
Natural Gas	MBtu	400,000.0	360,000.0	40,000.0	600,000.0

EMISSIONS REDUCTION SUMMARY

Energy type	Average Annual Emissions			Life-Cycle Reduction
	Base Case	Alternative	Reduction	
Electricity:				
CO2 (Kg):	3,005.0	0.0	3,005.0	45,075.1
SO2 (Kg):	10.9	0.0	10.9	163.6
NOx (Kg):	9.1	0.0	9.1	135.8
Natural Gas:				
CO2 (Mg):	21,125.3	0.0	21,125.3	316,879.9
SO2 (Kg):	84.0	0.0	84.0	1,260.0
NOx (Kg):	16,460.0	0.0	16,460.0	246,900.0
Total:				
CO2 (Mg):	21,128.3	0.0	21,128.3	316,925.0
SO2 (Kg):	94.9	0.0	94.9	1,423.6
NOx (Kg):	16,469.1	0.0	16,469.1	247,035.8

Figure 5. Comparative BLCC Analysis

The Technology in Perspective

The future of non-chemical water treatment technologies is promising. As public awareness of the environmental effects of chemicals increases there will be an increasing demand to deploy alternative, more environmentally beneficial technologies. As a means of reducing energy consumption and stretching the available personnel resources in the days of ever-shrinking budgets, non-chemical technologies make sense as both cost effective and having demonstrated performance.

The Technology's Development

Magnetic and electrical effects on water were first noticed prior to the turn of the 20th century. Considerable research is being conducted on magnetohydrodynamics by the Japanese as a means of propulsion, and similar research has been conducted in the past in the United States and other industrialized countries. This research has been facilitated by the advent of rare earth magnets, solid state electronics, and advanced ceramic or polymeric materials after World War II. Only after these advances has non-chemical water treatment shown promise and come into more widespread use.

Of the manufacturers listed in this FTA most have come into existence since the advent of the environmental movement in the United States in the early 1970s. This can be attributed both to the advent of cost-effective components (e.g., magnets, electronics) and to the public desire for more "green" or environmentally friendly alternatives to chemical treatment.

Relation to Other Technologies

The use of the non-chemical technologies does not prohibit the use of any other technology or equipment. As was mentioned previously, the change from chemical to non-chemical scale control may warrant investigation of other means of corrosion or biofouling control, as these three chemical scale treatment or control strategies or applications are often balanced amongst each other.

An increase in cycles of concentration was also noted by one user as another water saving measure that was employed. The ability to increase the cycles of concentration was attributed to the stability of scale-forming ions or scale particles in suspension. Water consumption was halved in this multi-pass system.

Technology Outlook

There is no basis to assume that the technologies are going to disappear anytime soon. Each has a historical basis of successful installations. Advances in materials science should only serve to improve each of the technologies. More powerful magnets will allow the magnetic devices to become smaller and/or more efficacious. More durable electrodes and dielectric compounds will improve the life of the electrostatic units.

Probably the most significant trend is the move away from chemical treatment technologies. This trend has begun at the consumer level, is becoming apparent at the corporate level, and will continue to grow. Increased availability of information on the technologies, the environment, and human health will only serve to feed this trend.

Manufacturers

The following is a listing of manufacturers of these technologies compiled from the Thomas Register and those who have contacted FEMP directly. It has been limited to U.S. manufacturers; foreign manufacturers or U.S. affiliates of foreign manufacturers were not included. No effort was made to locate and include manufacturers not listed in the Thomas Register. This listing does not purport to be complete, to indicate the right to practice the technology, or to reflect future market conditions.

Advanced Environmental Products

9450 Schulman #113

Dallas, TX 75243

214/340-1435

Fax: 214/344-2134

Aqua-Floe Inc.

Department T-94

6244 Frankford Avenue

Baltimore, MD 21206

800/368-2513

410/485-7600

Fax: 410/488-2030

Aqua Magnetics International, Inc.

915-B Harbor Lake Drive

Safety Harbor, FL 34695

813/447-2575

Fax: 813/726-8888

Conservonics

30555 Southfield Road #420

Southfield, MI 48076

801/540-3634

Fax: 810/716-7508

Descal-A-Matic Corp

4855-T Brookside Ct. Suite A

Norfolk, VA 23502

757-858-5593
Fax: 757/853-3321
Electrostatic Technologies Inc.
2223 Guinotte Avenue
Kansas City, MO 64120
816/842-0616
Fax: 816/842-9756
Enecon Corp.
125 Bayliss Road Suite 190
Mellville, NY 11747-3800
800/854-1374
Enertec Inc.
Department TR
306 Railroad Street
P.O. Box 85
Union City, MI 49094
517/741-5015
Fax: 517/741-3474
Hydrodynamics Corp.
1615 W. Abram Street #110
Arlington, TX 76013
817/277-6700
Fax: 817/277-2197
Magnatech Corp.
Superior Manufacturing Division
2015 S. Calhoun Street
P.O. Box 13543
Fort Wayne, IN 46868
800/692-1123
219/456-3596
Fax: 219/456-3598
Progressive Equipment Corp.
419 East 9th Street
Erie, PA 16503
814/452-4363
800/728-6395
Fax: 814/459-3094
Quantum Magnetic Systems Inc.
5224 Blanche Ave.

Cleveland, OH 44127
216/441-9670
Fax: 216/441-9677
Zeta Hydrometals Corporation
4565 S. Palo Verde Road, Suite 213
Tucson, AZ 85714
520/747-4550
888/785-9660
Fax: 520/747-4454

Who is Using the Technology

Federal Sites

Included here are but a few of the installations provided by the manufacturers. For a full listing the reader is advised to contact a manufacturer directly. Some manufacturers expressed concern about printing customer names in a public list such as this Federal Technology Alert but indicated they could provide such customer references to interested potential buyers. Most manufacturers specify having hundreds to almost 10,000 installations. Not all of these sites were contacted during the course of preparing this FTA.

GSA, Suitland, MD

National Aeronautics and Space Administration, multiple locations
United States Coast Guard, multiple locations

United States Air Force, Luke AFB, Phoenix, AZ

United States Army Corps of Engineers, Sacramento District, Sacramento, CA

United States Environmental Protection Agency, Andrew W. Breidenbach Environmental Research Center, Cincinnati, OH (Rich Koch and Bob Banner, Cleveland

Telecommunications Corporation)

United States Postal Service, multiple locations

Non-Federal Sites

Arnold Printing, Cincinnati, OH (Hank Majeushi, 513/533-9600)

Bethlehem Steel, multiple locations
Chrysler, multiple locations

Ford Motor Company, multiple locations

General Electric, multiple facilities

General Motors, multiple facilities

Getty Center, Los Angeles, CA

Inland Steel, 200 locations
House of the Future, Ahwatukee, AZ (Arnold Roy, The Frank Lloyd Wright Foundation, 602/948-6400)
John Deere, multiple locations
John Hancock Center, Chicago, IL
LTV Steel, multiple locations
Protective Coatings Inc. (Bob Bernadin and Ron Byers, 219/456-3596)
National Steel, over 100 installations
USX, multiple locations
United States Playing Card Company, Cincinnati, OH (Tom Berens, 513/396-5700)

For Further Information

Associations

No trade associations exist that are specific to the non-chemical water treatment technology manufacturers. The following associations are general water quality associations.

American Water Works Association

6666 West Quincy Ave
Denver, CO 80235
303/794-7711

Cooling Tower Institute

P.O. Box 73383
Houston, TX 77273
713/583-4087

Water Quality Association

4151 Naperville Road
Lisle, IL 60532
708/505-0160

Consultants

Robert A. Marth
340 Central Avenue
Sunnyvale, CA 94086
408/746-0964
Fax: 408-737-0291

T. Craig Molden
Water Service Technology/NWI
P.O. Box 545 Michigan City, IN 46361
219/879-8425
Fax: 219/879-8852

User and Third Party Field Test Reports

The following references represent only a small sample of the published work on these technologies. The references here are intended to give the reader an indication of the history of scientific research on the topic as well as the sponsoring agencies and interested audiences.

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Gruber and Carda. 1981. *Performance Analysis of Permanent Magnet Type Water Treatment Devices*. South Dakota School of Mines and Technology. Sponsored by and protocol by Water Quality Association.

Hibben, S.G. 1973. *Magnetic Treatment of Water*. Advanced Research Projects Agency of the Department of Defense.

Marth, R.A. 1997. *A Scientific Definition of the Magnetic Treatment of Water: Its Subsequent Use in Preventing Scale Formation and Removing Scale*. Research Conducted for Descal-A-Matic Corporation.

Parsons, S.A., Bao-Lung Wang, S.J. Judd, and T. Stephenson. 1997. "Magnetic Treatment of Calcium Carbonate Scale -- Effect of pH Control." *Water Research*, 31(2): 339-342.

Quinn, C.J., T.C. Molden, and C.W. Sanderson. 1996. "Nonchemical Approach to Hard Water Scale, Corrosion and White Rust Control." In *Proceedings Iron and Steel Engineer*, Chicago IL, September 30, 1996.

Reimers, R.S., P. S. DeKernion, and D. B. Leftwich. 1979. "Sonics and Electrostatics - An Innovative Approach to Water and Waste Treatment." In *Proceedings Water Reuse Symposium*, Volume 2. American Water Works Research Association Research Evaluation, Denver, CO.

Rubin, A.J. 1973. *To Determine if Magnetic Water Treatment is Effective in Preventing Scale*. The Ohio State University, Columbus, OH.

Schmutzer, M. A., and G. W. Hull. 1969. *Examination to Determine the Physical or Chemical Differences Between Untreated and Magnetically Treated Water*. United States Testing Center, Inc. Hoboken, NJ.

Simpson, L. G. 1980. "Control Scale and Save Energy." *The Coast Guard Engineer's Digest*, Volume 20, Number 205, pp. 32-35.

Design and Installation Guides

Many of the manufacturers have guides for internal use or use by their recommended installer or sales agent. Contained in these guides are listings of customers, design and installation notes, warranty information, and answers to many user questions. Most or all of this information may not be available to customers. However, the manufactures do make available sales brochures and summaries of specific applications or case studies. Also included with the units will be owner's manuals and other end user installation and maintenance documentation.

Appendixes

Appendix A: Federal Life-Cycle Costing Procedures and the BLCC Software

Appendix B: Life-Cycle Cost Analysis Summary

Contacts

General Contacts

Ted Collins
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Program Manager
Federal Energy Management Program
U.S. Department of Energy

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